

REMARKS

This Preliminary Amendment cancels the original claims, without prejudice, in the underlying PCT Application No. PCT/DE02/04193. The Preliminary Amendment also adds new claims 10-18. The new claims conform the claims to U.S. Patent and Trademark Office rules and do not add new matter to the application.

In accordance with 37 C.F.R. § 1.125(b), the Substitute Specification (including the Abstract) contains no new matter. The amendments reflected in the Substitute Specification (including Abstract) are to conform the Specification and Abstract to United States Patent and Trademark Office rules or to correct informalities. As required by 37 C.F.R. §§ 1.121(b)(3)(ii) and 1.125(c), a Marked-Up Version of the Substitute Specification comparing the Specification of record and the Substitute Specification also accompanies this Preliminary Amendment. Approval and entry of the Substitute Specification (including Abstract) are respectfully requested.

The underlying PCT Application No. PCT/DE02/04193 includes an International Search Report, dated September 22, 2003, a copy of which is submitted herewith.

Applicant asserts that the subject matter of the present application is new, non-obvious, and useful. Prompt consideration and allowance of the application are respectfully requested.

Respectfully submitted,

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CIRCUIT ARRANGEMENT FOR BRIEFLY MAINTAINING AT LEAST
ONE INTERNAL NORMAL D.C. VOLTAGE UPON FAILURE OF THE
VEHICLE ELECTRIC SYSTEM SUPPLY VOLTAGE

Field Of The Invention

The present invention is directed to a circuit arrangement of the type defined in the definition of the species in Claim 1.

5 Background Information

To an increasing extent, electronic circuits in the automotive field must be able to fulfill a full or restricted scope of functions (sending messages to telephone modules for emergency calls, deployment of airbags, etc.) for a certain period of time (reserve power time) after the vehicle electric supply voltage has been shut down or the battery has been disconnected (e.g., in a
10 collision).

In control units today, the power required for this is typically stored temporarily in a capacitor. According to the equation $W = \frac{1}{2} C U^2$, this power is proportional to capacitance C of the capacitor and the square of voltage U . To minimize capacitance C of the capacitor and
15 be able to store a large amount of power, the capacitor is usually charged to a voltage which is higher than the vehicle electric system supply voltage, via a step-up regulator, which is generally designed as a switching regulator.

In the event of loss of power supply voltage, power is taken from the reserve energy capacitor
20 via one or more step-down regulators which generate the required internal normal d.c. voltage(s).

This is explained in greater detail below with reference to Figure 1 of the drawing.

25 Figure 1 shows a circuit arrangement known from the related art in a highly schematized style, with vehicle electric system supply voltage V_{BAT} being supplied to the voltage input at

the left in the figure via a non-reversible diode 1 and the voltage output at the right in the figure delivering an internal normal d.c. voltage V_{CC} which is usually lower than vehicle electric system supply voltage V_{BAT} for the power supply to downstream electronic circuits (not shown).

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To be able to maintain internal normal d.c. voltage V_{CC} for at least a short period of time in the event of failure of vehicle electric system supply voltage V_{BAT} so that at least some of the downstream electronic circuits will be able to continue operating satisfactorily, the known circuit arrangement includes an energy storage mechanism designed as a capacitor 3, which is charged to a voltage distinctly higher than vehicle electric system supply voltage V_{BAT} during regular operation to minimize the size of capacitor 3 for cost reasons and nevertheless store as much power as possible in it, and thus be able to bridge the gap for the longest possible period of time in the event of an emergency. To generate a much higher charging voltage for capacitor 3 from vehicle electric system supply voltage V_{BAT} , a step-up regulator 5 is situated between non-reversible diode 1 and capacitor 3, the output voltage of this step-up regulator functioning in regular operation as the charging voltage for capacitor 3 and also as input direct voltage V_{ZP} for a step-down regulator 7, which generates from this input direct voltage V_{ZP} normal d.c. voltage V_{CC} which is actually needed.

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In an emergency, from reserve voltage V_{RES} which is supplied by capacitor 3 and is high at first but then drops continuously, this step-down regulator 7 maintains normal d.c. voltage V_{CC} for as long as possible.

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Step-down regulator 7 is part of a closed loop including a comparator (not shown) which compares internal normal d.c. voltage V_{CC} with a predetermined setpoint value and including a final controlling element (not shown) which supplies step-down regulator 7 with a control signal that varies as a function of the voltage difference detected by the comparator.

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Two fundamentally different types of such step-down regulators are known.

First, a linear regulator may be used here, including a longitudinal transistor whose on-state voltage is varied so that it is equal to the required difference between input direct voltage V_{ZP} and internal normal d.c. voltage V_{CC} which is to be established. This procedure takes place in

regular operation and also during emergency operation in which input direct voltage V_{ZP} is then equal to progressively declining reserve voltage V_{RES} delivered by capacitor 3. The simple design of such a linear regulator is advantageous, but it has the disadvantage that during emergency operation it causes a power loss for at least as long as reserve voltage V_{RES} is significantly higher than internal normal d.c. voltage V_{CC} that is to be established.

As an alternative, a switching regulator whose longitudinal transistor is alternately completely conducting or completely blocked with the help of triggering pulses may also be used here. Depending on the size of input direct voltage V_{ZP} , the pulse duty factor of the triggering pulses is varied, so that required internal normal d.c. voltage V_{CC} is obtained at a downstream smoothing capacitor. This is advantageous in emergency operation in particular because the power losses remain low regardless of the size of input direct voltage $V_{ZP} = V_{RES}$, but this comes at the expense of a much greater circuit complexity.

Step-up regulator 5 is required in the related art but it has a number of other disadvantages apart from the complex circuitry and the increased space required. For example, it requires an inductance which is difficult to implement as an integrated circuit and it creates an additional power loss which has a negative effect on the efficiency of the arrangement and increases the complexity for dissipation of the heat thus generated. It also has a negative effect on the EMC properties of the arrangement because it increases EMC emissions.

Advantages of the Summary Of The Invention

The circuit arrangement according to the present invention having the features of Claim 1 has the advantage that a step-up regulator may be omitted completely in a "high-voltage vehicle electric system." This prevents the associated power losses and greatly improves the efficiency of the overall arrangement. Less heat is generated, so this reduces the complexity required for dissipating heat. This arrangement is easily integratable because it does not contain any inductors. Emission of interference signals is reduced and less circuit board area is required while the overall cost is reduced due to the reduction in components.

~~Other advantages of the present invention are achieved through the measures characterized in the subclaims.~~

~~Drawing~~

Brief Description Of The Drawings

Figure 1 shows a known circuit arrangement for briefly maintaining at least one internal normal d.c. voltage for electronic circuits in the event of failure of the vehicle electric system supply voltage.

~~Exemplary embodiments~~ Figure 2 shows a circuit arrangement according to an exemplary embodiment of the present invention ~~are depicted in Figures 2 and 3.~~

Figure 3 shows a circuit arrangement according to another exemplary embodiment of the present invention.

Detailed Description

In the circuit arrangements according to the present invention as depicted in Figures 2 and 3, the same reference numbers are used for circuit elements that are included in the same way as in the arrangement shown in Figure 1.

Each of the two circuit arrangements depicted in Figures 2 and 3, both highly schematized, receives a vehicle electric system supply voltage V_{BAT} via a non-reversible diode 1, but this vehicle electric system supply voltage comes from a “high-voltage vehicle electric system” amounting to 42 V, for example. According to the present invention, this voltage is applied directly to capacitor 3, which functions as an energy storage mechanism, because no step-up transformation is necessary since it is already a high voltage. As explained in greater detail below, this is also the case in the exemplary embodiment depicted in Figure 3.

In addition, each of the two circuit arrangements depicted in Figures 2 and 3 has at least one step-down regulator 7 generating at least one internal normal d.c. voltage V_{CCI} from its high input direct voltage V_{ZP} (which in emergency operation is equal to reserve voltage V_{RES} supplied by capacitor 3).

In embodiments that are particularly preferred, other step-down regulators 8, 9, etc. may be connected in parallel with this at least one step-down regulator 7 so that voltage V_{ZP} which is supplied to them by non-reversible diode 1 in normal operation and reserve voltage V_{RES} which is supplied by capacitor 3 in emergency operation (or a voltage derived from this in the

case of Figure 3) are supplied to them as an input direct voltage while they deliver another internal normal d.c. voltage V_{CC2} , V_{CC3} , etc. at their respective outputs, this voltage in each case being used for power supply by a separate group of downstream electronic circuits. Individual internal normal d.c. voltages V_{CC1} through V_{CC3} may have the same and/or different values.

Here again, each step-down regulator 7 through 9 shown here is part of a closed loop, as already explained above with reference to Figure 1.

The exemplary embodiment according to Figure 3 differs from that in Figure 2 in which reserve voltage V_{RES} delivered by capacitor 3 is applied directly to step-down regulator(s) 7 through 9 in that in addition to step-down regulator(s) 7 through 9 here, an upstream step-down regulator 11 is also provided between the output of non-reversible diode 1 and capacitor 3. This upstream step-down regulator 11 is designed so that in regular operation it applies the voltage coming from non-reversible diode 1 unchanged, i.e., in particular without step-up transformation, to capacitor 3, as indicated by broken line arrow F. However, in emergency operation, this step-down regulator regulates reserve voltage V_{RES} which is delivered by capacitor 3 and steps it down progressively to the extent that input direct voltage V_{ZP} which is supplied to the at least one step-down regulator 7 and/or a plurality of step-down regulators 7 through 9 is constantly only slightly above normal d.c. voltage V_{CC1} through V_{CC3} which is the greatest to be generated.

This has the great advantage that only upstream step-down regulator 11 need be designed as a comparatively complex switching regulator, while downstream step-down regulators 7 through 9 may be formed by simple and inexpensive linear regulators at which in emergency operation there are no major power losses because of the minor voltage differences between their inputs and outputs due to upstream step-down regulator 11, thus permitting optimum utilization of the reserve power stored in capacitor 3.

In regular operation, upstream step-down regulator 11 remains completely blocked in the downward direction and is completely open in the upward direction, i.e., from non-reversible diode 1 to capacitor 3. This yields the special advantage that particularly high charge levels, which are supplied to capacitor 3 through voltage excesses occurring in the vehicle electric

system, are maintained at least as long as capacitor 3 has not discharged to the regular level of voltage coming from non-reversible diode 1 due to parasitic creep currents. In those cases, when a failure of vehicle electric system supply voltage V_{BAT} has occurred within a short period of time after a voltage rise, a particularly high and long-lasting reserve power is available.

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List of Reference Notation

	1	non-reversible diode
	3	energy storage mechanism
5	5	step-up regulator
	7	step-down regulator
	8	step-down regulator
	9	step-down regulator
	11	upstream step-down regulator
10	V_{BA}	vehicle electric system supply voltage
	V_T	
	V_{CC}	general internal normal d.c. voltage
	V_{CC1}	first internal normal d.c. voltage
	V_{CC2}	second internal normal d.c. voltage
15	V_{CC3}	third internal normal d.c. voltage
	V_{RES}	reserve voltage
	V_{ZP}	input direct voltage

Abstract Of The Disclosure

A circuit arrangement is described, to which the vehicle electric system supply voltage (V_{BAT}) is applied and which for briefly maintaining at least one internal normal d.c. voltage ($V_{ECT, \dots}$) in the event of failure of the vehicle electric system supply voltage (V_{BAT}) includes an reserve energy accumulator (3) to which a charging voltage higher than the at least one internal normal d.c. voltage is applied in regular operation and which in the event of failure of the vehicle electric system supply voltage delivers a reserve voltage (V_{RES}) with which operation of at least some electronic circuits may be maintained for a limited period of time, and it includes at least one step-down regulator (7,...) which steps down the applied input direct voltage (V_{ZP}) to the at least one internal normal d.c. voltage ($V_{ECT, \dots}$). In regular operation the supply direct voltage is applied directly as a charging voltage to the reserve energy accumulator and is also applied as the input direct voltage to the step-down regulator.

Figure 2